

RF Performance of Planar III–V Nanowire-Array Transistors Grown by Vapor–Liquid–Solid Epitaxy

Kelson D. Chabak, Xin Miao, Chen Zhang, *Student Member, IEEE*, Dennis E. Walker, Jr., *Member, IEEE*, Parsian K. Mohseni, and Xiuling Li, *Senior Member, IEEE*

Abstract—The radio frequency (RF) performance of a III–V transistor comprised of nanowire (NW) high-electron mobility channels, grown by planar vapor–liquid–solid epitaxy in parallel arrays, is examined. An equivalent small-signal circuit model was used to study the contributing extrinsic and intrinsic passive elements on the NW performance as a function of bias and gate length (L_G). Adequate intrinsic gain (g_m/g_{ds}) ~ 25 with low intrinsic (R_i) and terminal resistances (R_G , R_S , R_D) lead to an $f_T/f_{max} \sim 30/78$ GHz for $L_G = 150$ nm and NW diameter ~ 160 nm. The gate capacitance (C_g) is extracted and $\sim 2/3$ of the total C_g is parasitic, which can be reduced with denser NW arrays. Excellent agreement between measured and modeled RF performance is achieved.

Index Terms—Nanowire, parallel-array, radio frequency, transistor, small-signal model, vapor-liquid-solid.

I. INTRODUCTION

III–V NANOWIRES (NWs) for electronic devices are emerging due to their inherent three-dimensional (3D) geometry, which can be utilized as a multiple gate, high-mobility channel with enhanced electrostatic gate-channel coupling [1]. Attention has especially been given to NWs grown by metal-seeded vapor-liquid-solid (VLS) epitaxy as this eliminates damage from top-down etching. Immediate benefits of III–V NWs, so far, have focused on improved static performance over conventional transistors [2]–[7]. Realizing high-speed NW performance requires densely packed arrays of NWs aligned in parallel so that the overall intrinsic gate capacitance ($C_{g,i}$) is large compared to the total parasitic capacitance ($C_{g,p}$) [8]. By doing so, high-speed 3D NW channels with enhanced electrostatics are candidates for future RF nanoelectronics with high maximum oscillating frequency (f_{max}) [9]. However, the practical challenges of

NW assembly have resulted in low f_{max} , and the RF behavior of nanoscale channels has been left largely unexplored. For example, the record RF speed for laterally aligned InAs and silicon VLS NWs is 1.8 GHz [5] and 0.34 MHz [10], respectively, while the best carbon nanotube transistor has reached just 30 GHz [11]—all far below their theoretical potential. Major contributing factors for low f_{max} include the fringing fields of the gated regions between NWs, which do not conduct in the on-state but still contribute to $C_{g,p}$. One solution is to leave dense arrays of VLS NWs in their preferred out-of-plane growth direction, but this creates high pad capacitance from overlapping transistor terminals [4]. Alternatively, an f_{max} exceeding 300 GHz with 32-nm gate length (L_G) has also been achieved with III–V non-planar channels aligned in the substrate plane via selective regrowth [12]. In that case, the channel geometry depends on top-down lithography; whereas, bottom-up NWs grown by VLS method require patterning only the metal seed nanoparticle.

Recently, we reported wafer-scale assembly of high-speed, defect-free planar NWs as high-electron mobility transistor (HEMT) channels, grown self-aligned in dense, parallel arrays along the substrate surface by the planar VLS method [13]. In this letter, we present an in-depth study of the RF performance and use a small-signal equivalent circuit model (SSM) to investigate the limiting and contributing factors for high f_{max} using planar-array NW-HEMT channels. RF characterization of NW-HEMTs as a function of L_G and bias are discussed in detail.

II. DEVICE FABRICATION AND RF MEASUREMENTS

Two-finger AlGaAs/GaAs NW-HEMT devices were grown and fabricated on a (100) semi-insulating (SI) GaAs wafer using a process described in [13] and [14]. For this sample, the NW diameter is ~ 160 nm with 300-nm patterned NW center pitch. As illustrated in Figs.1(a)–(c), the GaAs NWs grow bi-directionally on this substrate orientation so only about half of the parallel NWs are used for the HEMT fabrication. The number of NWs per device is ~ 25 , each of which spans across both sides of the double channels; and the T-gate L_G varies from 150–300 nm in 50 nm increments. For $L_G = 150$ nm and $V_{DS} = 2$ V, the dc metrics are 0.2 mA/ μ m maximum drain current, 0.35 mS/ μ m peak transconductance ($g_{m,peak}$), $I_{ON}/I_{OFF} \sim 10^4$, $V_{TH} \sim +0.2$ V, $SS \sim 102$ mV/dec and $DIBL \sim 140$ mV/V [13].

RF performance was characterized with an Agilent E8364B parametric analyzer equipped with bias tees for dc bias. Scattering (S -) parameters for each device were measured at various gate and drain bias in the 0.01–40 GHz range

Manuscript received February 11, 2015; revised March 20, 2015; accepted March 23, 2015. Date of publication March 30, 2015; date of current version April 22, 2015. This work was supported in part by the Electrical, Communications and Cyber Systems through the National Science Foundation under Award 1001928 (KDC, XM and XL), in part by the Division of Materials Research under Award 1006581 (CZ, PKM, and XL), and in part by the Air Force Research Laboratory, Sensors Directorate, Wright-Patterson AFB, OH, USA. The review of this letter was arranged by Editor L. Selmi.

K. D. Chabak is with the Department of Electrical and Computer Engineering, University of Illinois Urbana-Champaign, Champaign, IL 61820 USA, and also with the Air Force Research Laboratory, Wright-Patterson AFB, OH 45433 USA (e-mail: kelson.chabak.1@us.af.mil).

X. Miao, C. Zhang, P. K. Mohseni, and X. Li are with the Department of Electrical and Computer Engineering, University of Illinois Urbana-Champaign, Champaign, IL 61820 USA (e-mail: xiuling@illinois.edu).

D. E. Walker, Jr., is with the Air Force Research Laboratory, Sensors Directorate, Wright-Patterson AFB, OH 45433 USA.

Color versions of one or more of the figures in this letter are available online at <http://ieeexplore.ieee.org>.

Digital Object Identifier 10.1109/LED.2015.2416978

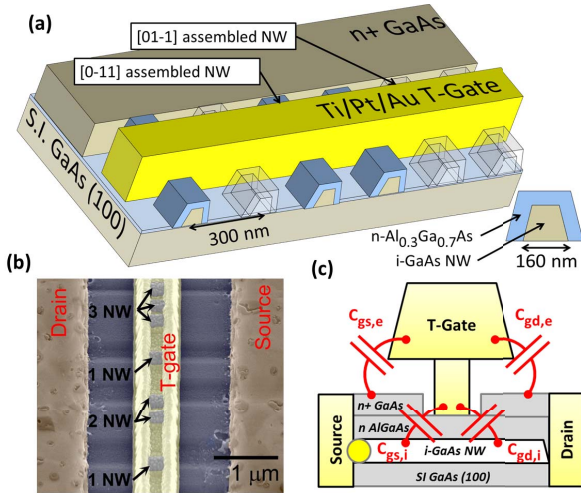


Fig. 1. (a) NW-HEMT device schematic in the gate recess region depicting the bi-directional VLS GaAs NW self-assembly on SI GaAs (100) substrate. Approximately half of the NWs are used for transistor fabrication. (b) Magnified top-view false color SEM of the NW-HEMT channel region. (c) A capacitive diagram of the NW-HEMT illustrating both extrinsic and intrinsic gate capacitance.

at -27 dBm power. Calibration to the RF probe tips was accomplished by short-open-load-thru routine with an off-chip substrate standard. Extrinsic pad delay was de-embedded with on-wafer open and short devices which resemble an identical NW-HEMT without the NWs and mesa.

III. RF MODEL AND RESULTS

The SSM illustrated in Fig.2(a) was used to examine the limiting and contributing factors for high-speed operation. Three bias conditions were used to isolate the extrinsic and intrinsic elements—(i) cold bias ($V_{GS}/V_{DS} = -2/0$ V), (ii) zero-bias ($V_{GS} = V_{DS} = 0$ V) and (iii) hot bias ($V_{GS}/V_{DS} = +0.6/2$ V). The extraction routine is the same as for conventional Schottky-gated III-V HEMTs, which uses a least squares fit after calculating an accurate starting estimate [15]. After determining the extrinsic components, the intrinsic circuit elements were analytically calculated. The resulting SSM values for $V_{GS} = +0.6$ V and $V_{DS} = +2$ V are displayed in Fig. 2(a).

Figs.2(b)-(d) illustrate the variation of extracted SSM parameters as a function of V_{GS} , V_{DS} and L_G , respectively. The gate capacitances, C_{gs} and C_{gd} , are greatly affected by both drain and gate bias because of the close proximity of the gate-recessed n^+ GaAs cap to the T-gate stem, just tens of nanometers as confirmed by cross-sectional scanning electron microscopy (SEM). The source and drain access resistance (R_S , R_D) was in the range of 25-35 Ω for the studied L_G range. The R_S is excellent considering the extracted intrinsic transconductance, $g_{m,i} \sim 3-6$ mS, results in $R_S \cdot g_{m,i} \ll 1$ and the measured transconductance, $g_m = g_{m,i}/(1 + R_S \cdot g_{m,i})$, is not greatly affected. Low Ti/Pt/Au T-gate resistance (R_G) increased incrementally from 100-188 $\Omega \cdot \mu\text{m}$ as L_G decreased. The intrinsic resistance (R_i) was the most volatile parameter which followed closely with the gate diode leakage. For example, R_i was the highest as V_{DS} and V_{GS} approached 0 V and +0.7 V, respectively, which

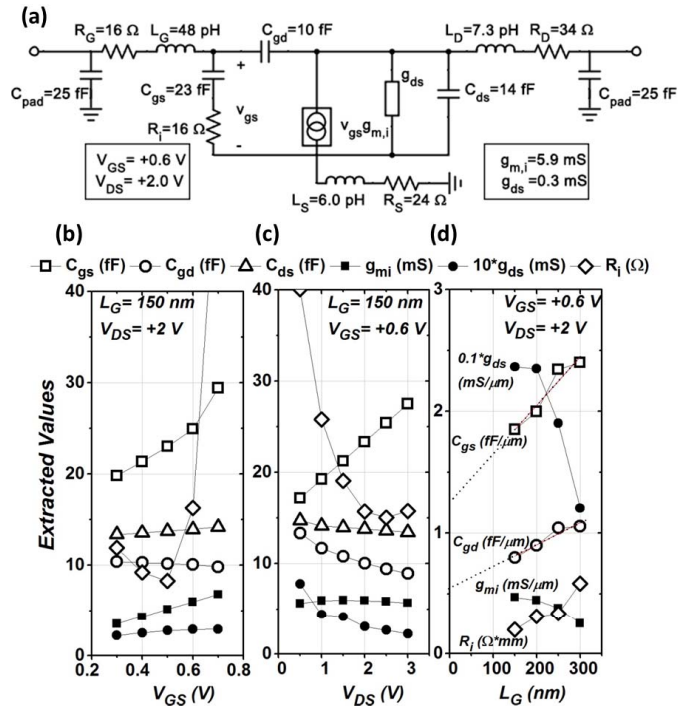


Fig. 2. (a) SSM for the fabricated NW-HEMT devices with approximately ~ 25 NWs each. The extracted values shown are for $L_G = 150$ nm at a bias of $V_{GS}/V_{DS} = +0.6/2.0$ V. (b)-(d) Influential extracted SSM parameters for high f_{max} as a function of V_{GS} , V_{DS} and L_G . In (d), the values are normalized to the total NW width.

is the two-terminal bias condition for forward-bias Schottky gate leakage. The optimal R_i occurs when the electron channel is formed at higher V_{DS} but with $V_{GS} < +0.7$ V to prevent the gate diode from turning on. The output conductance, g_{ds} , remains low for the entire biasing range, which is due to the excellent electrostatics afforded by the 3D NW channel multi-gate. The intrinsic gain, $g_o = g_{m,i}/g_{ds}$, an important figure of merit for high f_{max} (Fig.3(a)) clearly shows improvement with V_{DS} . For $L_G = 150$ nm, a high $g_o \sim 25$ was extracted. The significance of low terminal and intrinsic resistances combined with low output conductance for high f_{max} is given by eq.(1) below:

$$f_{max} = \frac{f_T}{2\sqrt{g_{ds}(R_G + R_i + R_S) + 2\pi f_T R_G C_{gd}}} \propto \frac{g_m}{\sqrt{g_m + g_{ds}}} \quad (1)$$

The current gain cutoff frequency, $f_T \approx g_m/(2\pi C_g)$, requires large g_m/C_g ratio where $C_g = C_{g,i} + C_{g,e}$ and $C_{g,e}$ is the extrinsic fringing gate capacitance. Both $C_{g,i}$ and $C_{g,e}$ can be separated into gate-source ($C_{gs,i}$ and $C_{gs,e}$) and gate-drain ($C_{gd,i}$ and $C_{gd,e}$) components as illustrated in Fig.1(c).

For the $L_G = 150$ nm NW-HEMT device, the $C_{g,i}$ and $C_{g,e}$ were extracted and analyzed. The L_G -independent $C_{g,e}$ can be extracted from the intercept of a C_g versus L_G plot in Fig.2(d). For each gated device, the C_g is normalized by taking the three-sided gated perimeter of each NW multiplied by the number of NWs. $C_{gs,e}$ and $C_{gd,e}$ were found to be 15.8 fF and 6.8 fF, respectively. The slope of C_{gs} and C_{gd} versus L_G defines the L_G -dependent elements, $C_{gs,i}$ and $C_{gd,i}$, which

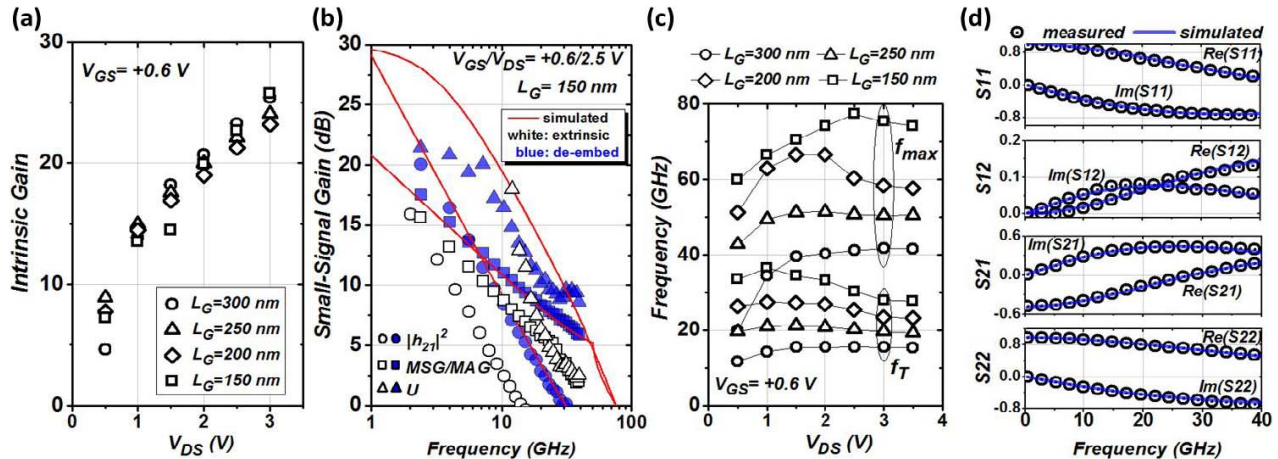


Fig. 3. (a) Intrinsic gain of the NW-HEMT device for various L_G and V_{DS} . (b) Representative extrinsic and de-embed RF gain performance for $L_G = 150$ nm and $V_{GS}/V_{DS} = +0.6/2.5$ V. (c) De-embed RF performance versus V_{DS} and L_G at $V_{GS} = +0.6$ V. (d) Excellent agreement between simulated and measured S -parameters is achieved using the values shown in the previously shown SSM circuit.

are 7.5 fF and 3.5 fF, respectively. When comparing these values to the total extracted C_{gs} and C_{gd} in Fig.2(c), we find $C_{gs,i}/C_{gs}$ and $C_{gd,i}/C_{gd}$ are 33% and 35%, respectively. In other words, $\sim 2/3$ of the total extracted C_g is parasitic. Most of $C_{g,p}$ is likely caused by the bi-directional VLS NW growth which can be optimized on (110) GaAs substrate orientation for uni-directional NW assembly and immediately enhance the g_m/C_g ratio for higher f_T/f_{max} [16].

The SSM values were used to simulate the maximum available and stable gains (MAG/MSG) and the de-embedded f_T and f_{max} . Fig.3(b) shows representative measured and de-embedded small-signal gain performance for $L_G = 150$ nm at $V_{DS} = +2.5$ V. Fig. 3(c) illustrates the dependence of f_T and f_{max} as a function of L_G and V_{DS} . The optimum f_T occurs at $V_{DS} = +1$ V, which is just beyond the saturation V_{DS} . For higher V_{DS} , the drain-side electric field degrades f_T likely because of impact ionization onset but also widens the drain depletion region to lower C_{gd} and increase f_{max} . The best frequency performance was measured at $V_{DS} = +2.5$ V with $f_T/f_{max} \sim 30/78$ GHz for $L_G = 150$ nm. An $f_{max} \cdot L_G \sim 11.7$ GHz $\cdot\mu\text{m}$ is the best reported among all NW and nanotube transistors [4], [5], [11], [12]. The total intrinsic delay, τ_i , can be estimated by $C_{g,i}/g_{m,i} = 1.86$ ps, and the corresponding electron velocity, v_e , is $L_G/\tau_i = 0.8 \cdot 10^7$ cm/s. Removing the fringing capacitance, a theoretical f_T can be determined by $(2\pi \cdot \tau_i)^{-1} = 85$ GHz. Using $f_{max} \approx [f_T/(8\pi \cdot R_G \cdot C_{gd,i})]^{0.5}$, a theoretical $f_{max} = 248$ GHz is calculated for the NW-HEMT device with $L_G = 150$ nm. Outstanding agreement between the measured S -parameters and the simulated S -parameters developed from Fig.2(a) is shown in Fig.3(d) and validates the SSM extraction process.

IV. CONCLUSION

The RF performance and SSM of a III-V NW-HEMT with densely aligned parallel AlGaAs/GaAs NWs have been presented. The NW-HEMT array has the highest $f_{max} = 78$ GHz reported for VLS NWs aligned along the substrate surface. The high f_{max} is attributed to low device resistance and good intrinsic gain. High $C_{g,p}$ limiting

RF performance can be improved with device engineering and unidirectional planar VLS NW growth on future samples.

REFERENCES

- [1] L.-E. Wernersson *et al.*, "III-V nanowires—Extending a narrowing road," *Proc. IEEE*, vol. 98, no. 12, pp. 2047–2060, Dec. 2010.
- [2] S. A. Fortuna and X. Li, "GaAs MESFET with a high-mobility self-assembled planar nanowire channel," *IEEE Electron Device Lett.*, vol. 30, no. 6, pp. 593–595, Jun. 2009.
- [3] X. Miao and X. Li, "Scalable monolithically grown AlGaAs–GaAs planar nanowire high-electron-mobility transistor," *IEEE Electron Device Lett.*, vol. 32, no. 9, pp. 1227–1229, Sep. 2011.
- [4] K.-M. Persson *et al.*, "Extrinsic and intrinsic performance of vertical InAs nanowire MOSFETs on Si substrates," *IEEE Trans. Electron Devices*, vol. 60, no. 9, pp. 2761–2767, Sep. 2013.
- [5] T. Takahashi *et al.*, "Parallel array InAs nanowire transistors for mechanically bendable, ultrahigh frequency electronics," *ACS Nano*, vol. 4, no. 10, pp. 5855–5860, Sep. 2010.
- [6] K. Tomioka, M. Yoshimura, and T. Fukui, "A III-V nanowire channel on silicon for high-performance vertical transistors," *Nature*, vol. 488, no. 7410, pp. 189–192, Aug. 2012.
- [7] C. Zhang and X. Li, "Planar GaAs nanowire tri-gate MOSFETs by vapor–liquid–solid growth," *Solid-State Electron.*, vol. 93, pp. 40–42, Mar. 2014.
- [8] J. C. Tinoco *et al.*, "Impact of extrinsic capacitances on FinFET RF performance," *IEEE Trans. Microw. Theory Techn.*, vol. 61, no. 2, pp. 833–840, Feb. 2013.
- [9] F. Schwierz and J. J. Liou, "RF transistors: Recent developments and roadmap toward terahertz applications," *Solid-State Electron.*, vol. 51, no. 8, pp. 1079–1091, Aug. 2007.
- [10] M.-G. Kang *et al.*, "Microwave characterization of a field effect transistor with dielectrophoretically-aligned single silicon nanowire," *Jpn. J. Appl. Phys.*, vol. 49, no. 6S, p. 06GG12, 2010.
- [11] M. Steiner *et al.*, "High-frequency performance of scaled carbon nanotube array field-effect transistors," *Appl. Phys. Lett.*, vol. 101, no. 5, pp. 053123-1–053123-4, 2012.
- [12] C. B. Zota *et al.*, "Radio-frequency characterization of selectively regrown InGaAs lateral nanowire MOSFETs," *IEEE Trans. Electron Devices*, vol. 61, no. 12, pp. 4078–4083, Dec. 2014.
- [13] X. Miao *et al.*, "High-speed planar GaAs nanowire arrays with $f_{max} > 75$ GHz by wafer-scale bottom-up growth," *Nano Lett.*, accepted for publication.
- [14] X. Miao, C. Zhang, and X. Li, "Monolithic barrier-all-around high electron mobility transistor with planar GaAs nanowire channel," *Nano Lett.*, vol. 13, no. 6, pp. 2548–2552, May 2013.
- [15] R. G. Brady, C. H. Oxley, and T. J. Brazil, "An improved small-signal parameter-extraction algorithm for GaN HEMT devices," *IEEE Trans. Microw. Theory Techn.*, vol. 56, no. 7, pp. 1535–1544, Jul. 2008.
- [16] R. S. Dowdy, D. A. Walko, and X. Li, "Relationship between planar GaAs nanowire growth direction and substrate orientation," *Nanotechnology*, vol. 24, no. 3, p. 035304, 2013.